

## Memo

To  
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**Subject**  
Use of the L/H ratio rule

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The WT12017 will allow a level 1 assessment ('*eenvoudig*'), in order to rule out "obviously safe" cases. This level 1 assessment can be based on a simple rule (*L/H* ratio) calibrated for the Dutch conditions using probabilistic analyses (memo 1220084-001-GEO-0001). The recommendations of the *L/H* ratio study were:

- As no significant difference (benefit) was observed when clustering per Region or Return period, and since this is intended to be a simple rule, it is recommended to use the *L/H* rule derived from the 20% quantile of all cases:
  - $L/H_{ratio} = 17 \beta_{T,cross} - 29$
- Furthermore, a somewhat more effective rule can be given as an option, which distinguishes between situations with thick layer and without cover layer:
  - No cover layer:  $L/H_{ratio} = 16 \beta_{T,cross} - 19$
  - Thick cover layer (>6m):  $L/H_{ratio} = 17 \beta_{T,cross} - 48$
  - Thin cover layer (0-6m):  $L/H_{ratio} = 17 \beta_{T,cross} - 29$  (same as all cases)

### How to use the *L/H* ratio rule in a practical case:

For each cross-section under study:

- For this cross-section the piping parameters are also known, namely the seepage length and the head difference between water levels, *L* and *H* respectively.
- The location is known, therefore the segment to which this cross-section and the safety standard can be taken from the Deltaprogramma 2015, e.g.: segment 15-1, return period  $T = 3,000$ .
- Transform this return period (*T*) into a required reliability at cross-section level ( $\beta_{T,cross}$ ), using the following formulas:

$$\beta_{T,cross} = \Phi^{-1}(1 - P_{T,cross})$$

Where

$$P_{T,cross} = \frac{P_T}{\left(1 + \frac{a \cdot L_{segm}}{b}\right)} = \frac{f \cdot 1/T}{\left(1 + \frac{a \cdot L_{segm}}{b}\right)}$$

Herein:

- $\beta_{T,cross}$  Cross sectional reliability requirement (reliability index) [-]
- $P_{T,cross}$  Cross-sectional target failure probability; the average cross-sectional probability of failure may not exceed  $P_{T,cross}$  [ $\text{yr}^{-1}$ ]
- $P_T$  Target failure probability: target probability of flooding due to the series of events triggered by the instability of the inner slope that lead to flooding [ $\text{yr}^{-1}$ ]
- $a$  Fraction of the length that is sensitive to the failure due to piping [  $a = 0.75$  ]
- $b$  Length-effect factor for piping failure [  $b = 300$  m ]
- $L_{segm}$  Total length of the dike segment
- $f$  is the failure probability factor (faalruimtefactor): target contribution of the failure mode (in this case piping) to the probability of flooding [  $f = 0.24$  ]
- $T$  Return period that corresponds to the safety standard of a segment [yr]

For more information on the length-effect and transformation of the requirements from a segment to a cross-section level refer to reports: 1207805-004-ZWS-005, 1202123-002-GEO-0005, 1220080-002-ZWS-0006.

As such:

- The L/H ratio present in the cross-section under assessment has to be bigger than  $L/H_{ratio} = 17 \beta_{T,cross} - 29$

More explicitly:

$$(L/H_{ratio})_{existing} \geq (L/H_{ratio})_{rule}$$

$$(L/H_{ratio})_{existing} \geq 17 \beta_{T,cross} - 29$$

$$(L/H_{ratio})_{existing} \geq 17 \cdot \Phi^{-1}(1 - P_{T,cross}) - 29$$

$$(L/H_{ratio})_{existing} \geq 17 \cdot \Phi^{-1}\left(1 - \frac{0.24 \cdot 1/T}{1 + 0.0025 \cdot L_{segm}}\right) - 29$$

Where the variables  $L$ ,  $H$ ,  $T$  and  $L_{segm}$  are known.